

Figure 2. Rectified projection data is subject to increasingly strong distortion as the primary angle difference between the two projections increases. Example of a typical circular CT trajectory of a Siemens Artis Zeego: (1) little distortion up to $\approx 45^\circ$, (2) considerable distortion at $\approx 90^\circ$, (3) method is beginning to break down after $\approx 135^\circ$, and (4) rectification not sensible for opposing views.

homogeneous coordinates $\mathbf{c}_0 \cong (C_0^0, C_0^1, C_0^2, 1)^\top \in \text{null}(\mathbf{P}_0)$ and \mathbf{c}_1 , accordingly, define the stereo baseline, where \cong denotes equality up to scale, define the stereo baseline. Its direction $\mathbf{d} \in \mathbb{S}^2$ is the unit vector

$$\mathbf{d} \cong \begin{pmatrix} C_2^0 - C_0^0 \\ C_1^1 - C_0^1 \\ C_1^2 - C_0^2 \end{pmatrix}, \quad (1)$$

where \cong denotes equality up to positive scalar multiplication. Its moment shall be the unit vector $\mathbf{m} \in \mathbb{S}^2$

$$\mathbf{m} \cong \begin{pmatrix} C_2^0 \\ C_1^1 \\ C_1^2 \end{pmatrix} \times \begin{pmatrix} C_0^0 \\ C_0^1 \\ C_0^2 \end{pmatrix}, \quad (2)$$

which is the normal to the plane which contains both the baseline and the origin.

B. Rectification by Re-Projection

Our goal is to project both images to a virtual detector with an image u -axis pointing in the direction of the stereo baseline. Assuming that the iso-center is approximately in the coordinate origin, a good choice of virtual detector plane is

$$\mathbf{e} \cong \begin{pmatrix} \mathbf{d} \times \mathbf{m} \\ 0 \end{pmatrix} \in \mathbb{P}^3. \quad (3)$$

Since the u -axis must point in direction of the baseline, we establish a 2D coordinate frame for points in the plane \mathbf{e} with 3D coordinate axis directions \mathbf{d} and \mathbf{m} according to

$$\mathbf{S} = \begin{pmatrix} \mathbf{d}^\top & 0 \\ \mathbf{m}^\top & m \end{pmatrix} \in \mathbb{R}^{3 \times 4}. \quad (4)$$

with arbitrary pixel size m in mm. Given an original image with projection matrix \mathbf{P} and source position $\mathbf{c} \in \text{null}(\mathbf{P})$, let $\mathbf{T}_c^e \in \mathbb{R}^{4 \times 4}$ denote the central projection through \mathbf{c} to 3D points on the virtual detector plane \mathbf{e} (compare Section II-C) and \mathbf{S} defined its 2D coordinate system. Then, the homography

$$\mathbf{H} = \mathbf{S} \mathbf{T}_c^e \mathbf{P}^+ \in \mathbb{R}^{3 \times 3}, \quad (5)$$

directly relates pixels from the original image with pixels in the virtual detector plane \mathbf{e} . This situation is visualized in Figure 1.

C. Central Projection onto a Plane

Central projection from a point $\mathbf{c} \in \mathbb{P}^3$ to a plane $\mathbf{e} \in \mathbb{P}^3$ can be written in a single matrix $\mathbf{T}_c^e \in \mathbb{R}^{4 \times 4}$. It projects a point $\mathbf{x} \in \mathbb{P}^3$ to a point $\mathbf{T}_c^e \mathbf{x} \in \mathbb{P}^3$ by intersection of the plane \mathbf{e} with the line \mathbf{r} through the points \mathbf{c} and \mathbf{x} . Using the Plücker matrix [2] of the line $\mathbf{c}\mathbf{x}^\top - \mathbf{x}\mathbf{c}^\top$ we express the intersection as

$$\mathbf{T}_c^e \mathbf{x} = \mathbf{c}\mathbf{x}^\top \mathbf{e} - \mathbf{x}\mathbf{c}^\top \mathbf{e}. \quad (6)$$

By factoring out \mathbf{x} we obtain the projection

$$\mathbf{T}_c^e = \mathbf{I}_4 \mathbf{c}^\top \mathbf{e} - \mathbf{c}\mathbf{e}^\top, \quad (7)$$

We can rectify two projections with the homographies

$$\begin{aligned} \mathbf{H}_0 &= \mathbf{S} \mathbf{T}_{c_0}^e \mathbf{P}_0^+ \\ \text{and } \mathbf{H}_1 &= \mathbf{S} \mathbf{T}_{c_1}^e \mathbf{P}_1^+. \end{aligned} \quad (8)$$

III. THE RADON TRANSFORM OF PERSPECTIVELY DISTORTED FUNCTIONS

A. Line Integrals in Perspectively Transformed Images

This section computes an integral along a line l' over an image which has been projectively transformed by a homography \mathbf{H} . We will express the integration over a line $l = \mathbf{H}^\top l'$ (see in Eq. 12) in the original image, weighted by the Jacobian. Let l be the line with angle to the u -axis α and signed distance to the origin τ

$$l \cong \begin{pmatrix} l_0 \\ l_1 \\ l_2 \end{pmatrix} = \begin{pmatrix} \sin(\alpha) \\ -\cos(\alpha) \\ -\tau \end{pmatrix}. \quad (9)$$

We append a zero to the 2D vectors of its normal $\mathbf{n} = (l_0, l_1, 0)^\top$ and direction

$$\mathbf{d} = \begin{pmatrix} d_0 \\ d_1 \\ 0 \end{pmatrix} = \begin{pmatrix} l_1 \\ -l_0 \\ 0 \end{pmatrix}, \quad (10)$$

with unit length $\|\mathbf{n}\| = \|\mathbf{d}\| = 1$. The closest point to the origin is given by the homogeneous coordinates

$$\mathbf{o} \cong \begin{pmatrix} o_0 \\ o_1 \\ 1 \end{pmatrix} = \begin{pmatrix} -l_2 l_0 \\ -l_2 l_1 \\ 1 \end{pmatrix}. \quad (11)$$

Lines transform covariantly, therefore, the transformed line is given by

$$\mathbf{H}^{-\top} l \cong l' = \begin{pmatrix} l'_0 \\ l'_1 \\ l'_2 \end{pmatrix} = \begin{pmatrix} \sin(\alpha') \\ -\cos(\alpha') \\ -\tau' \end{pmatrix}, \quad (12)$$

with direction

$$\mathbf{d}' = \begin{pmatrix} l'_1 \\ -l'_0 \\ 0 \end{pmatrix}. \quad (13)$$

The Radon transform is the integral over a line in an image

$$\begin{aligned} \mathcal{R}f(\alpha, \tau) &= \mathcal{R}f(\mathbf{l}) = \int f(o_0 + d_0 \cdot t, o_1 + d_1 \cdot t) dt \\ &\stackrel{\text{def}}{=} \int f_1(t) dt, \end{aligned} \quad (14)$$

where $f_1(t)$ is the image defined over the 1D sub-space parametrized by the line-coordinate t . Since a projective transformation \mathbf{H} on the image is collinearity preserving, a mapping $\varphi(t) : t \mapsto t'$ must exist which fulfills

$$\mathcal{R}\mathbf{H}f(\alpha', \tau') = \mathcal{R}\mathbf{H}f(\mathbf{l}') = \int f_1(\varphi^{-1}(t')) dt', \quad (15)$$

where $\mathbf{H}f$ denotes the transformed image and t' is the line coordinate along the transformed line \mathbf{l}' . Equation 15 shows that only information on the original line f_1 is required for this computation of $\mathcal{R}\mathbf{H}f(\mathbf{l}')$. A change of variables with $t' = \varphi(t)$ yields

$$\mathcal{R}\mathbf{H}f(\mathbf{l}') = \int f_1(t) \frac{\partial}{\partial t} \varphi(t) dt. \quad (16)$$

B. Projection to Line Coordinates

The goal of this section is to find a closed form for $\varphi(t)$ in Equation 15, by considering only the line coordinate t on the line \mathbf{l} and t' on the line \mathbf{l}' . Because the Jacobian of a rigid transformation is one, we can consider w.l.o.g. the case of $\mathbf{l}_u = (0, 1, 0)^\top$, which is related to the line \mathbf{l} with the rigid transformation

$$\mathbf{H}_{\mathbf{l}_u} = \begin{pmatrix} l_1 & -l_0 & 0 \\ l'_0 & l_1 & l_2 \\ 0 & 0 & 1 \end{pmatrix} \text{ with } \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = \mathbf{H}_{\mathbf{l}_u}^{-\top} \mathbf{l}. \quad (17)$$

Here, $\mathbf{H}_{\mathbf{l}_u}$ takes image points $\mathbf{x} = (u, v, 1)^\top$ on the line \mathbf{l} in the domain of the image $f(u, v)$ to line coordinates in the domain of $f_1(t)$

$$\mathbf{x} = \mathbf{o} + \mathbf{d}t = \mathbf{H}_{\mathbf{l}_u}^{-1} \begin{pmatrix} t \\ 0 \\ 1 \end{pmatrix} \text{ with } \mathbf{x}^\top \mathbf{l} = 0. \quad (18)$$

Analogously, we can transform line coordinates on \mathbf{l}' with $\mathbf{H}_{\mathbf{l}'_u}$ according to

$$\begin{pmatrix} t' \\ 0 \\ 1 \end{pmatrix} = \mathbf{H}_{\mathbf{l}'_u} \mathbf{x}' \text{ iff. } \mathbf{x}'^\top \mathbf{l}' = 0. \quad (19)$$

However, if \mathbf{H} is a rectifying homography according to Equation 8 and if \mathbf{l} is an epipolar line, then $\mathbf{d}' = (1, 0, 0)^\top$ by definition and $\mathbf{H}_{\mathbf{l}'_u}$ is only a translation.

C. Line-Induced Perspectivity

Using Equations 18 and 19 we have

$$\begin{aligned} \mathbf{x}' &\cong \mathbf{H}\mathbf{x} \\ \iff \mathbf{H}_{\mathbf{l}'_u}^{-1} \begin{pmatrix} t' \\ 0 \\ 1 \end{pmatrix} &\cong \mathbf{H}\mathbf{H}_{\mathbf{l}_u}^{-1} \begin{pmatrix} t \\ 0 \\ 1 \end{pmatrix} \\ \iff \begin{pmatrix} t' \\ 0 \\ 1 \end{pmatrix} &\cong \underbrace{\mathbf{H}_{\mathbf{l}'_u} \mathbf{H} \mathbf{H}_{\mathbf{l}_u}^{-1}}_{\mathbf{J}} \begin{pmatrix} t \\ 0 \\ 1 \end{pmatrix}. \end{aligned} \quad (20)$$

Since both sides of the equation contain a zero-element, only the four corner elements of the the matrix \mathbf{J} are relevant. Note that $\mathbf{H}_{\mathbf{l}_u}^{-1}$ and $\mathbf{H}_{\mathbf{l}'_u}$ can be elegantly written by column, respectively, row vectors

$$\mathbf{H}_{\mathbf{l}_u}^{-1} = \begin{pmatrix} | & | & | \\ \mathbf{d} & \mathbf{n} & \mathbf{o} \\ | & | & | \end{pmatrix}, \quad (21)$$

and

$$\mathbf{H}_{\mathbf{l}'_u} = \begin{pmatrix} - & \mathbf{d}'^\top & - \\ - & \mathbf{l}'^\top & - \\ 0 & 0 & 1 \end{pmatrix}. \quad (22)$$

The entries of \mathbf{l} can be computed via Equation 20, while we are only interested in the case where \mathbf{H} is a rectifying homography and \mathbf{l} is an epipolar line, we have more compactly, $\mathbf{d}' = (1, 0, 0)^\top$ and

$$J_{00} = \mathbf{d}'^\top \mathbf{H}\mathbf{d} = h_{00}l_1 - h_{10}l_0, \quad (23)$$

$$J_{02} = \mathbf{d}'^\top \mathbf{H}\mathbf{o} = h_{02} - h_{00}l_0l_2, \quad (24)$$

$$J_{20} = (0, 0, 1) \cdot \mathbf{H}\mathbf{d} = h_{20}l_1 - h_{21}l_0, \quad (25)$$

$$J_{22} = (0, 0, 1) \cdot \mathbf{H}\mathbf{o} = h_{22} - h_{20}l_0l_2 - h_{21}l_1l_2. \quad (26)$$

Assuming that the horizon is not contained in the support of f , de-homogenization of the mapping from \mathbb{P}^1 coordinates on the line \mathbf{l} to \mathbb{P}^1 coordinates on the line \mathbf{l}' is written

$$t' = \varphi(t) = \frac{J_{00} \cdot t + J_{02}}{J_{20} \cdot t + J_{22}}, \quad (27)$$

and

$$\frac{\partial}{\partial t} \varphi(t) = \frac{J_{00}J_{22} - J_{02}J_{10}}{J_{20}^2 t^2 + 2 \cdot J_{20}J_{22} \cdot t + J_{22}^2}. \quad (28)$$

The Radon transform for a line \mathbf{l}' can thus be computed using regular ray-casting in f by weighting each sample $\mathbf{x} = \mathbf{o} + t \cdot \mathbf{d}$ with $\frac{\partial}{\partial t} \varphi(t)$. For some regular sampling distance Δt in the original image (typically about 0.66 px), we have

$$\mathcal{R}\mathbf{H}f(\mathbf{l}') \approx \Delta t \sum_i \frac{f(\mathbf{o} + t \cdot \mathbf{d}) \cdot (J_{00}J_{22} - J_{02}J_{10})}{J_{20}^2 t^2 + 2 \cdot J_{20}J_{22} \cdot t + J_{22}^2} \Big|_{t=i \cdot \Delta t}, \quad (29)$$

with the original line

$$\mathbf{l} \cong \mathbf{H}^\top \mathbf{l}' = \mathbf{H}^\top \begin{pmatrix} \sin(\alpha') \\ -\cos(\alpha') \\ -\tau' \end{pmatrix}. \quad (30)$$

IV. DISCUSSION

We have presented a general and fast algorithm for evaluation of fan-beam DCCs on a virtual detector plane based on Lesaint et al. [4], which also handles non-circular trajectories. We have shown that reprojection to a common virtual detector is an instance of stereo rectification. However, rectifying each pair of projections, requires $n \cdot (n - 1)$ rectified 2D images. In Figure 2 we show that rectification increasingly distorts the images, as the angle between the primary rays increases. For proper sampling rectified images would have to be considerably larger than the original projections, rendering the original algorithm impractical. We show how to compute line integrals over projectively transformed images on the fly, i.e. directly from the original projection image data, which is drastically faster and requires no additional memory. This

Algorithm 1 Radon transform of a projectively distorted image $\mathbf{H}f$ for a line $l' = \mathbf{H}^{-T}l$ from original image f .

- **input** – Line $l' = (\sin(\alpha'), -\cos(\alpha'), -\tau)^\top$
- Homography $\mathbf{H} \in \mathbb{R}^{3 \times 3}$ (as in Equation 8).

- 1) Compute l according to Equation 30, its closest point \mathbf{o} (Equation 11), and direction \mathbf{d} (Equation 10).
- 2) Normalize $\|\mathbf{n}\| = \|\mathbf{d}\| = 1$ and dehomogenize $o_2 = 1$.
- 3) Compute J_{00} to J_{22} according to Equations 23-26.
- 4) Compute values t_{min} and t_{max} , such that $\mathbf{x}_{min} = \mathbf{o} + t_{min} \cdot \mathbf{d}$ and $\mathbf{x}_{max} = \mathbf{o} + t_{max} \cdot \mathbf{d}$ are the intersections of the line with the image border with $t_{min} < t_{max}$.
- 5) Initialize summation variable s .
- 6) **for** ($t = t_{min}$; $t \leq t_{max}$; $t \leftarrow t + \Delta t$)
 - a) Compute pixel location $\mathbf{x} \leftarrow \mathbf{o} + t \cdot \mathbf{d}$
 - b) Compute $j \leftarrow \frac{\partial}{\partial t} \varphi(t)$ according to Equation 28.
 - c) Compute distance w of 3D location of \mathbf{x} (on the virtual detector) to the source position.[4], [5]
 - d) Increment $s \leftarrow s + f(\mathbf{x}) \cdot j \cdot w \cdot \Delta t$.
- 7) **return** Variable s , which is the Radon transform of projectively distorted image $\mathbf{H}f$ for a line l' .

paper gives a general implementation for this situation. For validation, we present in Figure 4, top, the redundant signals extracted from two X-ray shots of a pumpkin, along with the warped images in Figure 3. The fan-beam consistency condition can be computed explicitly as a sum over these rectified images weighted by the distance of each point to the stereo baseline. Integration in the original images, while taking into account the Jacobian according to Algorithm 1 is identical. The method breaks down for large primary angle difference, once the epipoles lie within the images, compare Figure 2, right. To demonstrate the fundamentally different nature of this consistency condition by comparison with epipolar consistency for the same epipolar planes in Figure 4, bottom. Since EC is based on a derivative orthogonal to the lines, we observe a roughly zero-mean curve and more detail for smaller structures. Generally speaking, rectification-based methods will be slower than their derivative-based counterparts for motion- and calibration-correction, because the Radon intermediate functions cannot be pre-computed. Future work will investigate, if avoidance of the derivative has potential benefits in applications, where absolute intensity values need to be estimated, such as beam-hardening, scatter correction or metal-artifact correction. Future work will investigate how the presented epipolar DCCs are affected by truncation and we will compare other DCCs.

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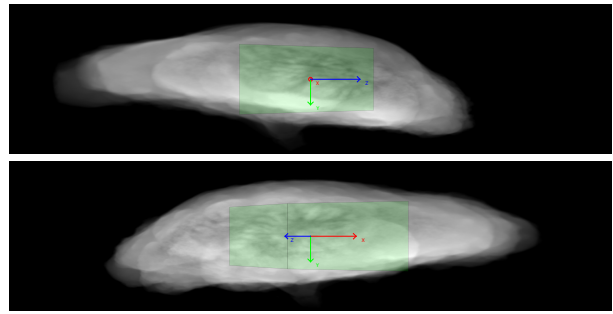


Figure 3. Rectified projection images of a pumpkin phantom in case of a primary angle difference of 120° . The green cube is intended to visualize the distortion introduced by rectification.

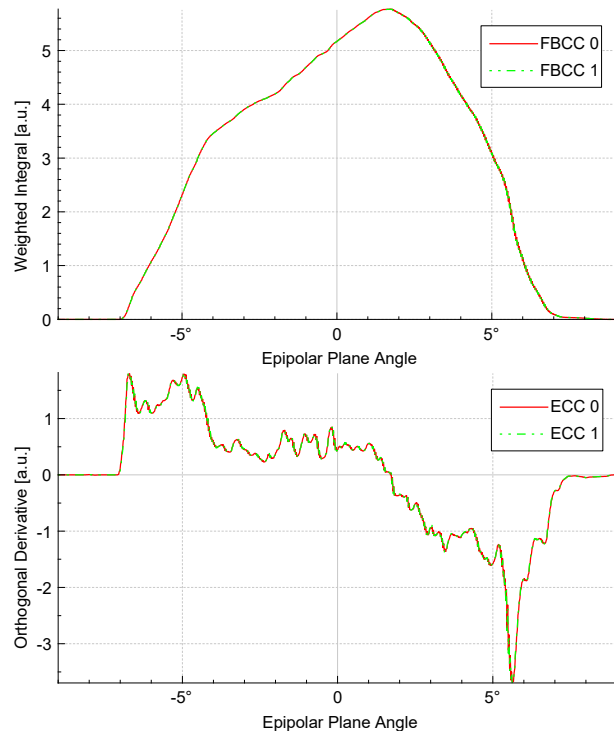


Figure 4. Top: Fan-beam consistency condition (FBCC) [5] as implemented in the original images. The computation of the rectified images in Figure 3 is avoided, but the curves are identical to a weighted summation over the intensity in these images. Bottom: Comparison to epipolar consistency conditions (ECC) for the same images (i.e. orthogonal derivative instead of rectification and weighting) is shown for corresponding epipolar plane angles.

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